

III–V/Silicon Photonics for Short-Wave Infrared Spectroscopy

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(Invited Paper)

Abstract—In this paper, we review our work on III–V/SOI photonic integrated circuits for short-wave infrared applications. We focus on the integration of short-wave infrared photodetectors on a silicon photonics platform and on the generation of a short-wave infrared supercontinuum using the $\chi^{(3)}$ nonlinearity in silicon photonic wires. In addition, the performance of a silicon optical parametric amplifier is reviewed, as a first step towards constructing an integrated tunable short-wave infrared parametric oscillator.

Index Terms—Heterogeneous integration, short-wave infrared, silicon photonics.

I. INTRODUCTION

THE SILICON photonics platform is broadly being studied as an attractive platform for the extremely dense integration of optical functions at telecommunication wavelengths [1]. The use of CMOS fabrication technology, leading to high yield and the potential for co-integration of electronic circuits, and the high refractive index contrast available on a silicon-on-insulator waveguide platform ($\Delta n \cong 2$) are the main drivers for this evolution. While photonic integrated circuits were primarily intended to serve the telecommunication and data-communication markets, the use of silicon photonics in other applications is also being explored, predominantly geared towards sensing. Examples of such fields of research

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are silicon-based bio-sensors [2], gas sensors [3] and the development of bio-medical instrumentation [4]. In these applications, one typically retains the use of the telecommunication wavelength range, for reasons of experimental simplicity, the availability of characterized building blocks, etc.

However, a number of applications would benefit from the use of highly integrated silicon photonic circuits specifically tailored to operate at longer wavelengths. For the specific field of spectroscopic sensing, probing of the molecular fingerprint absorption lines of molecules exploits the strong absorption features of molecules in the short-wave (1.4–3 μm) and mid-wave (3–8 μm) infrared [5]. The availability of an integration platform covering these two wavelength ranges could enable ultra-compact, low-cost sensor solutions, designed to outperform existing solutions in terms of their selectivity, sensitivity, portability, and power consumption.

In this paper we report on our first steps towards the development of such a long-wavelength silicon photonics platform, by addressing the 2–2.5 μm wavelength range. We will first focus our discussion to the heterogeneous integration of III–V short-wave infrared photodetectors on a silicon waveguide circuit as a milestone towards the realization of complete post-dispersive spectrometer chips [6]. We then also report on the use of the strong $\chi^{(3)}$ nonlinearity in silicon photonic wires to generate short-wave infrared radiation, in the form of an on-chip short-wave infrared supercontinuum or through on-chip optical parametric amplification and oscillation.

II. LONG WAVELENGTH III–V / SILICON PHOTONICS

Depending on the particular wavelength range of operation, standard silicon-on-insulator waveguide structures can be used with a silicon waveguide core layer on top of a SiO_2 cladding layer. While silicon is transparent to beyond 6 μm , the SiO_2 cladding limits the wavelength range of operation of the SOI waveguide platform to about 4 μm [7]. Alternative waveguide structures such as free-standing silicon membranes [8], silicon-on-sapphire [9], silicon-on-nitride [7], germanium-on-silicon [7] or silicon-on-porous silicon [10] need to be considered when wavelengths beyond 4 μm are of interest. While in the short-wave infrared, standard SOI waveguide structures can be used (note that in this paper a 220 nm silicon waveguide layer on top a 2 μm buried oxide layer was used), until recently the silicon waveguide platform has lacked light sources and photodetectors for this

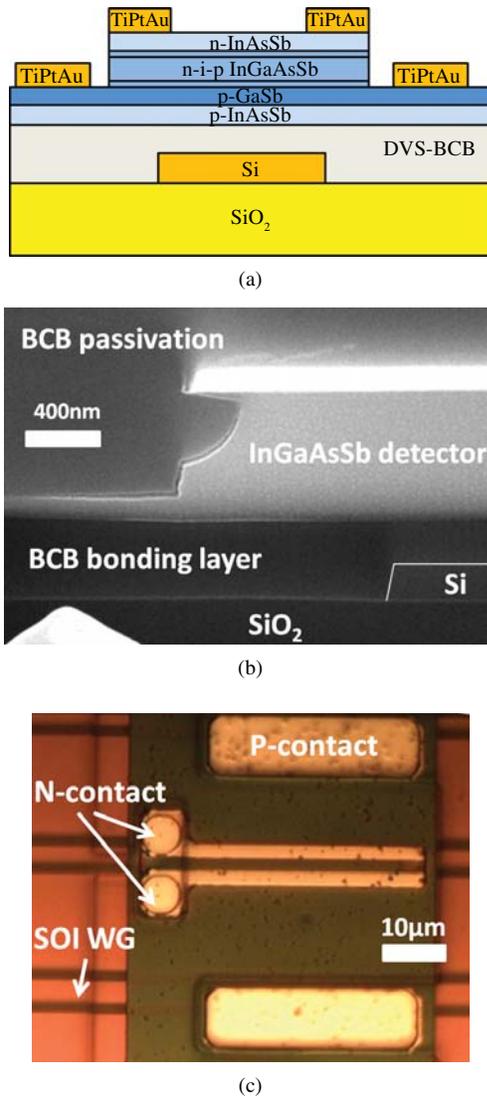


Fig. 1. (a) Schematic cross-section of the heterogeneous III-V/silicon photodetector. (b) SEM cross-section of the fabricated device. (c) Top-down microscope image of the InGaAsSb photodetector aligned to the underlying silicon waveguide circuit.

wavelength range. Therefore, a process for the integration of III-V semiconductors on top of the silicon waveguide circuits was developed, by means of epitaxial layer transfer with an adhesive bonding layer. This process was originally developed to transfer InP-based epitaxy to a silicon waveguide circuit for 1.3 μm to 1.7 μm applications. However, it is difficult to push the emission and/or absorption wavelength of InP/InGaAsP/InGaAlAs-based structures far beyond 2 μm [11]. Moreover, an alternative semiconductor system, the InP-based quantum cascade materials, typically address wavelengths beyond 4 μm [12]. Therefore, in this work a heterogeneous integration process for GaSb-based epitaxy was developed, which allows for band-to-band laser emission and photodetection in the 2–3.5 μm wavelength range [13].

To illustrate the heterogeneous integration process, InGaAsSb-based photodetectors were integrated on a silicon waveguide circuit. The device layout is shown in Figure 1(a) [14]. The GaSb-based epitaxial layer stack, grown using

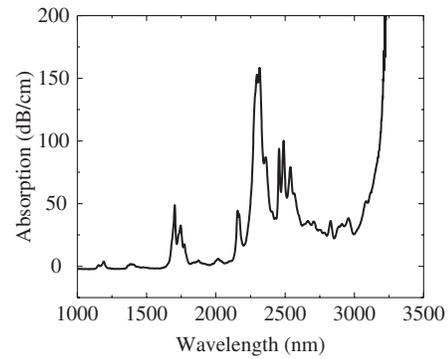


Fig. 2. Absorption spectrum of DVS-BCB in the short-wave infrared, measured using a photospectrometer setup.

molecular beam epitaxy on an n-type GaSb substrate, is bonded “upside down” onto the SOI waveguide wafer, using the same process as reported in [15], i.e. using a DVS-BCB adhesive bonding agent. After bonding, the GaSb growth substrate is removed by chemical wet etching with a mixture of HF, CrO₃ and water (1:1:3 v/v), using an InAsSb layer as an etch stop, which is in turn removed by a mixture of citric acid and hydrogen peroxide (2:1 v/v), leaving a III-V epitaxial film attached to the silicon waveguide circuit, in which the III-V opto-electronic components can be defined. The epitaxial stack consists of 50 nm p-InAsSb ($1.0 \times 10^{18} \text{ cm}^{-3}$), 50 nm p-doped ($1.0 \times 10^{18} \text{ cm}^{-3}$) GaSb and a 50 nm p-doped ($1.0 \times 10^{18} \text{ cm}^{-3}$) In_{0.21}Ga_{0.79}As_{0.19}Sb_{0.81} layer as the p-zone of a p-i-n layer stack. An un-intentionally doped 500 nm thick In_{0.21}Ga_{0.79}As_{0.19}Sb_{0.81} layer is used for the intrinsic absorbing region, and has a cut-off wavelength of 2.5 μm . The n-type region consists of In_{0.21}Ga_{0.79}As_{0.19}Sb_{0.81} and 50 nm InAs_{0.91}Sb_{0.09}. Both are doped to 10^{18} cm^{-3} . An InAs_{0.91}Sb_{0.09} layer is chosen as n-type contact because of its lower bandgap (0.35 eV) and low contact resistance.

The III-V mesa, 9 μm wide, was defined using a combination of both dry (CH₄:H₂) and wet etching to reduce the dark current of the photodetector. TiPtAu contacts were used both for n-type and p-type metallization. Figure 1(b) shows a SEM cross-section image of the integrated device while Figure 1(c) shows a top-down microscope image. The coupling from the silicon waveguide layer to the InGaAsSb photodetector is based on evanescent coupling between the SOI (3 μm wide and 220 nm high silicon core) and III-V waveguide. While DVS-BCB is considered transparent in the telecommunication wavelength band, there are strong absorption bands in the short-wave infrared as shown in Figure 2. This implies that the DVS-BCB needs to be removed on top of the silicon waveguide circuits to avoid excessive waveguide losses, leaving the DVS-BCB only underneath the bonded III-V opto-electronic components. Currently a process is under development such that by applying a 5–10 nm aluminum oxide layer on the silicon waveguide circuit prior to spin-coating of the DVS-BCB, this aluminum oxide can serve as an etch stop during the dry etch removal of the DVS-BCB bonding layer after III-V processing.

To characterize the short-wave infrared photodetectors, the light from a short-wave infrared tunable laser [16] was coupled

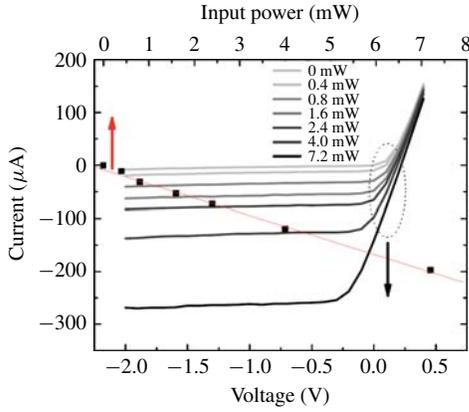


Fig. 3. I-V characteristics of the heterogeneously integrated short-wave infrared photodetector for different optical power levels in the silicon waveguide (2.25 μm -TE polarization) and photocurrent at 0.1 V bias for different input power levels.

to a standard single mode fiber (SMF), which interfaces with the silicon waveguide circuit, after passing a polarization controller, using a one-dimensional grating coupler designed for the short-wave infrared. While a basic grating design with limited efficiency was used for the characterization of the devices, a proper design of such gratings allows for efficient (-5 dB fiber-to-chip coupling efficiency experimentally obtained) and broadband (160 nm 3 dB bandwidth) coupling from a standard SMF to a single mode SOI waveguide [17]. The photodetector I-V curves at room temperature for various fiber-coupled power levels at 2.25 μm are shown in Figure 3. Calibrating and then correcting for the fiber-chip coupling efficiency, an on-chip responsivity larger than 0.4 A/W is obtained over a 200 nm wide band around 2.3 μm . The dark current at room temperature is 1.13 μA (-0.1 V bias). This leads to a Johnson-noise-limited noise equivalent power of 1.5 $\text{pW}/\text{Hz}^{1/2}$. From Figure 1 a slight misalignment between the photodetector and the underlying silicon waveguide circuit can be observed, which impacts the responsivity. In future device runs therefore higher responsivity can be expected.

III. GENERATION OF SHORT-WAVE INFRARED RADIATION THROUGH NONLINEAR OPTICS

In addition to photodetectors, a second component needed for a fully functional IR chip is a heterogeneously integrated short-wave infrared light source, mounted on the silicon waveguide platform. One possible approach would be to utilize the epitaxial layer transfer process described above to bond and lithographically define a GaSb-based semiconductor injection laser structure. Another valuable approach could make use of silicon nonlinear optical components specifically designed to generate broadband short-wave infrared radiation [18]–[21]. As will be shown in this section, the latter approach allows coverage of a much broader spectral range than what can be achieved with a single GaSb-laser epitaxial structure. The ultra-broadband characteristics of silicon nonlinear optical devices are very useful for spectroscopy applications. Of course, using nonlinear optics to generate broadband radiation still requires integration of a narrowband and bright optical

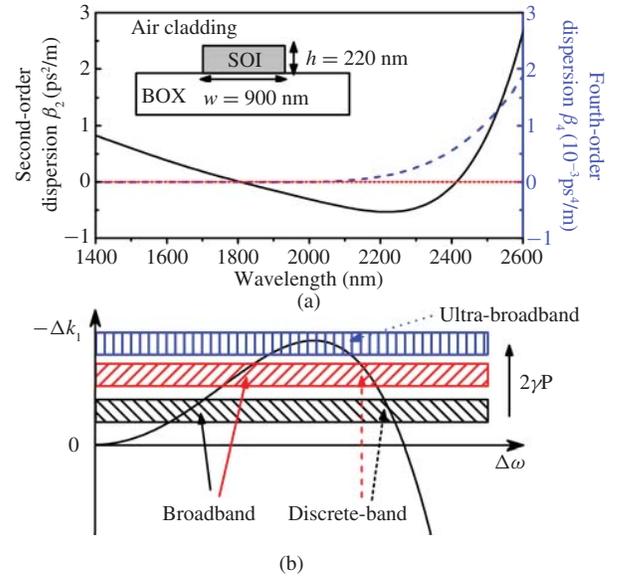


Fig. 4. (a) Second-order and fourth-order waveguide dispersion of the 900 nm 220 nm silicon photonic wire studied and graphical illustration of the phase matching condition. The curve shows the linear phase mismatch as a function of detuning from the pump. (b) Intersections with the horizontal boxes this linear phase mismatch is compensated by the nonlinear phase mismatch.

pump source on the chip, which could be realized using a heterogeneous InGaAsSb/SOI laser. In this section, we will focus on the basic nonlinear optical properties of silicon photonic wires in the short-wave infrared, after which we will demonstrate generation of a 1.5–2.5 μm supercontinuum and wide-band optical parametric generation / amplification on a silicon chip using picosecond optical pump pulses.

Prior to this work, silicon photonics for nonlinear optics at telecommunication wavelengths had been explored in depth [22]–[28]. This interest stems from the large bulk $\chi^{(3)}$ optical nonlinearity of silicon combined with the tight confinement of the optical mode in a single-mode waveguide, along with the large range of waveguide dispersion engineering that is possible with a single-mode Si wire waveguide [29]–[31]. At telecommunication wavelengths, silicon however exhibits parasitic two-photon absorption, which limits the efficiency of the nonlinear processes at these wavelengths. Given the 1.12 eV bandgap of silicon, this two-photon absorption process disappears above 2.2 μm , resulting in much higher efficiency nonlinear processes in the short-wave infrared [32]. For our nonlinear optics experiments here, 900 nm wide and 220 nm thick silicon strip wire waveguides are used with an air top cladding. The waveguide cross-section is shown in the inset of Figure 4(a). Using a cut back technique - by comparing the insertion loss of a 1 cm, 2 cm, 4 cm and 7 cm long spiral waveguides - the TE mode waveguide propagation loss is found to be approximately 2.5 dB/cm across the 2050–2450 nm wavelength range. Since the short-wave infrared wavelength generation relies upon phase matching of the interacting waves, waveguide dispersion engineering is of paramount importance. Indeed, efficient four-wave mixing (FWM) occurs only when

$$\Delta k = \Delta k_{lin} + \Delta k_{nonlin} = k_s + k_i - 2k_{pump} + 2\gamma P = 0 \quad (1)$$

in which k_{pump} , k_s and k_i are the linear propagation constants of the pump, signal and idler waves, respectively. The term $2\gamma P$, in which γ is the effective nonlinear parameter of the waveguide and P is the peak power of the pump pulse, accounts for the self-phase and cross-phase modulation of the interacting waves [31]. Using a Taylor expansion of the waveguide dispersion relation around ω_{pump} , and taking into account the conservation of energy in the FWM process, produces the phase matching condition

$$\beta_2 \Delta\omega^2 + \frac{1}{12} \beta_4 \Delta\omega^4 + 2\gamma P = 0 \quad (2)$$

in which $\Delta\omega$ is the frequency detuning between pump and signal (and also between pump and idler). The second- (β_2) and fourth-order (β_4) waveguide dispersion of the 900 nm wide photonic wire are plotted in Figure 4(a). Anomalous dispersion ($\beta_2 < 0$) is obtained in the 1800–2400 nm wavelength range, while β_4 is small but positive. The effective nonlinear parameter of this waveguide is calculated to be 130–150 (Wm)⁻¹ at short-wave infrared wavelengths.

The phase matching condition described by equations (1) and (2) is graphically illustrated in Figure 4(b). Given the opposite signs of β_2 and β_4 exhibited by the 900 nm × 220 nm waveguide design, Figure 4(b) shows that two phase-matched frequency bands can be obtained around two detuning frequencies. These bands are labeled as the broad and the discrete band, respectively. At these detunings the linear and nonlinear phase mismatch compensate each other. Due to the steepness of the linear phase mismatch curve far away from the pump, the bandwidth of the discrete band is smaller than that of the broad band close to the pump. Increasing the pump power eventually leads to the merging of both bands, at which point ultra-broadband phase-matching is obtained. This effect was exploited in a recent experiment, in which optical parametric generation over a 580 nm-wide wavelength band was demonstrated by sending a picosecond pulse train at 2.173 μ m wavelength with 13.5 W coupled peak input power through a 2-cm-long silicon photonic wire [33]. The optical parametric generation, shown in Figure 5(a), originates primarily from modulation instability, the amplification of background noise through ultra-broadband FWM with the pump. The intense modulation instability spectrum correlates with unprecedented values of on-chip parametric gain, exceeding 40 dB (Figure 5(c)). Moreover, we have demonstrated that on-chip gain can exceed 50 dB in narrow Raman-scattering-assisted bands, also shown in Figure 5(c). This gain spectrum was obtained by coupling a weak co-polarized continuous wave probe signal along with the pump pulse train, leading to the parametric amplification of the signal when the pump and signal overlap in time (hence the pedestal around the spiked continuous wave tones in Figure 5(b) on the red side of the pump) and the simultaneous generation of an idler pulse train. Taking into account the duty cycle of the pulse train (2 ps long pulses, 76 MHz repetition rate) the effective amplification and conversion gain can be calculated as shown in Figure 5(c).

In order to further understand the processes involved in the generation of this short-wave infrared radiation, the generation of a supercontinuum was studied at different pump power

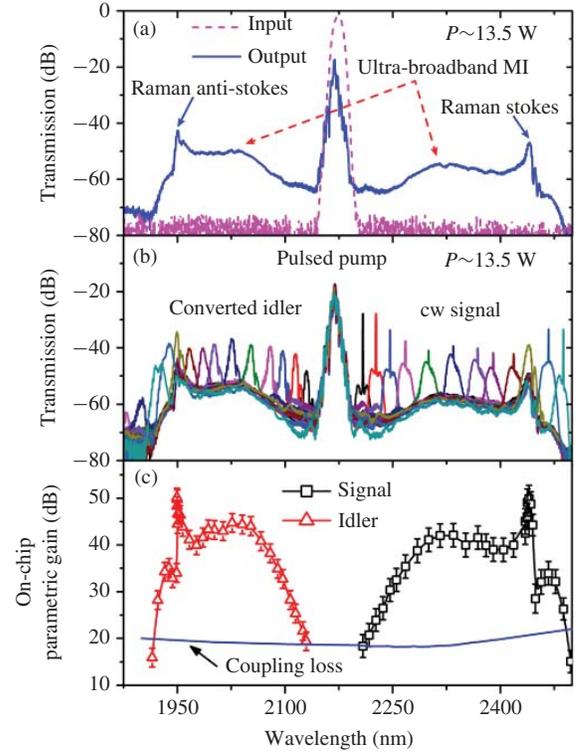


Fig. 5. (Color online) (a) Input (dashed magenta) and output (solid blue) pump spectrum, taken with an input peak power $P \sim 13.5$ W and $\lambda = 2173$ nm, illustrating ultra-broadband modulation instability. (b) Series of FWM spectra with the pulsed pump co-propagating with a cw mid-IR signal at various wavelengths. (c) Spectrum of on-chip parametric signal gain (black squares) and idler conversion gain (red triangles). Fiber-waveguide coupling loss is shown by the blue trace. The 3 dB gain bandwidth of the four-wave mixing process is about 100 nm around a wavelength of 2330 nm.

levels within the same silicon waveguide [34]. In this experiment, the picosecond pump pulses were centered at a slightly shorter wavelength near 2120 nm, as this pump wavelength was found to produce the broadest possible emission spectrum. The wavelength dependence of the extent of the supercontinuum is caused by the strong wavelength dependence of the second-order and fourth order dispersion terms as shown in Figure 4. The waveguide output spectra are shown in Figure 6 as the input coupled peak pump power is gradually increased from 3.1 W (green trace) to 12.7 W (black trace). As can be seen from this study, different nonlinear effects ultimately determine the shape and the extent of the generated supercontinuum. Even at the lowest input power, the pump pulse train's spectrum is broadened significantly by self phase modulation (SPM), as illustrated by the interference fringes appearing near 2120 nm. In turn, this phenomenon causes associated broadening of the sidebands generated through modulation instability and Raman scattering. The broadband and the discrete phase matched side-bands are labeled as MI(1) and MI(2), respectively. Spontaneous Raman scattering can also clearly be observed, red-shifted by 15.6 THz from the pump as expected. At a pump power of 7.9 W, several new spectral components are observed, peaked near 1700 nm and 1600 nm, respectively. The component at 1700 nm is generated through cascaded FWM, where the original MI(2) peak at

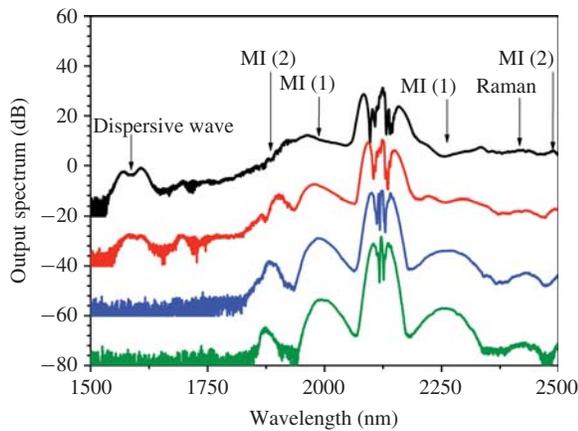


Fig. 6. Measured output spectrum for increasing values of coupled input peak power (color online) 3.1 W (green), 4.3 W (blue), 7.9 W (red), and 12.7 W (black). The spectra are vertically offset by multiples of 20 dB for clarity.

1890 nm serves as the degenerate pump and the input pulse at 2120 nm acts as the signal. The peak around 1600 nm is believed to be the result of Cherenkov radiation, also referred to as dispersive wave generation [35]. Measurement of the spectral content of the supercontinuum using a Fourier Transform Infrared spectrometer (FTIR) showed a long-wavelength cut-off at 2.55 μm .

In contrast to previous supercontinua generated using planar waveguide circuits, where high-power femtosecond pulses were required [36], the short-wave infrared supercontinuum demonstrated here is generated from picosecond pulses with moderate peak powers. The combination of the relaxed pump pulse requirements and the large supercontinuum spectral range makes the silicon wire waveguide platform attractive for development of highly integrated white light infrared sources for spectroscopic applications. Moreover, the large concurrent parametric gain exhibited also allows realization of a broadly tunable optical parametric oscillator in the short-wave infrared [37].

IV. CONCLUSION

In this paper we reported on our first steps in the field of long-wavelength silicon photonics. This research is fueled by the need for compact, integrated solutions for spectroscopic sensor systems in the MIR for biomedical applications and environmental monitoring, since many relevant molecules have “fingerprint” absorption lines within this wavelength range. The baseline for this research is the use of a CMOS compatible waveguide platform extended with III-V epitaxy for photodetectors. In a later stage integrated laser diodes will follow, which will rely on the bonding of a separate III-V die containing the laser epitaxy. The first successful demonstration of heterogeneously integrated short-wave infrared photodetectors on a silicon waveguide platform is reported, together with a comprehensive summary of the generation of short-wave infrared radiation through FWM in silicon photonic wires. These results show that there is a bright future for short-wave and mid-wave infrared photonic integrated circuits based upon

a combination of silicon and III-V semiconductor photonic technology.

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